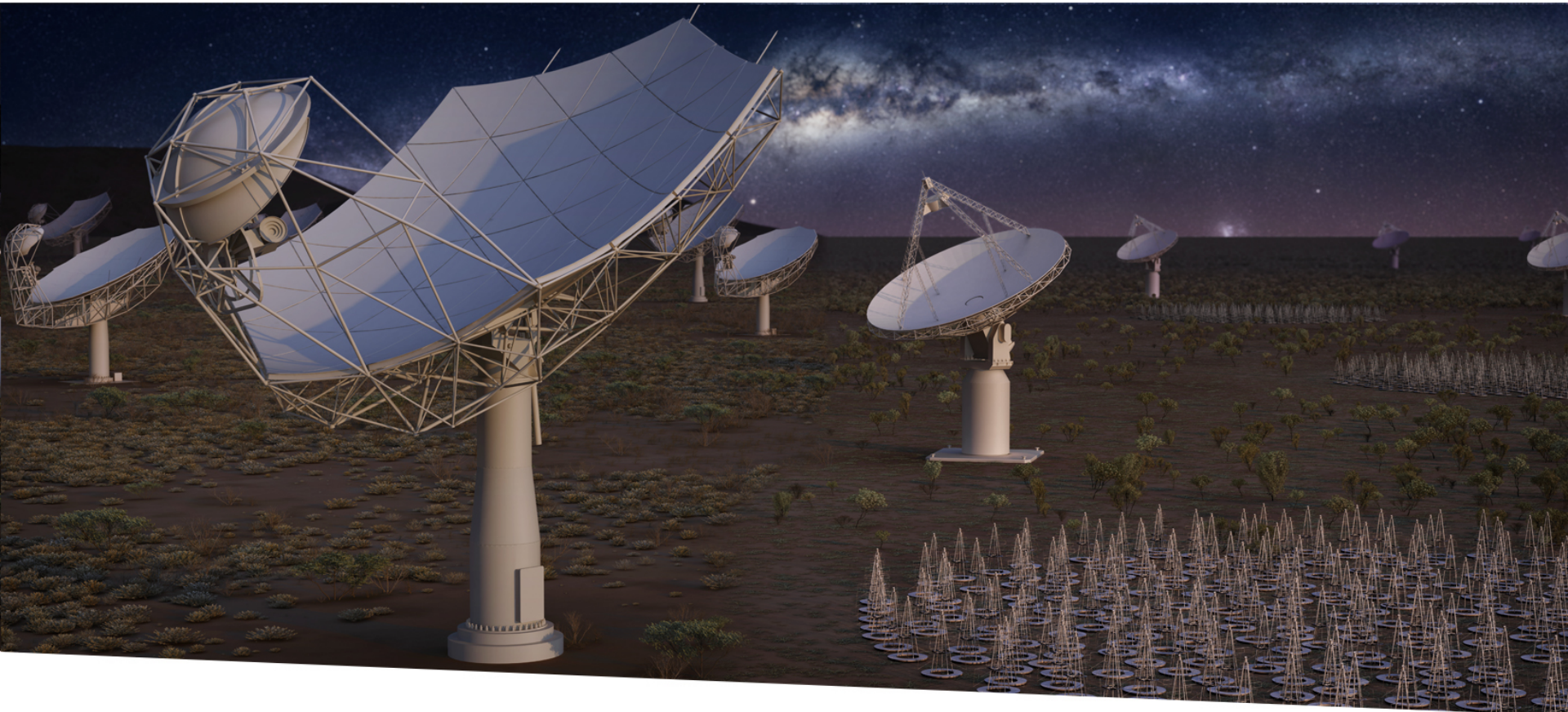


Electromagnetic modelling of the SKA-LOW AAVS2 prototype



SQUARE KILOMETRE ARRAY David Davidson & Pietro Bolli et al

Exploring the Universe with the world's largest radio telescope Sep 2020, URSI-GASS, Rome

Contributors

- *ICRAR-Curtin (Australia)*: David Davidson, Marcin Sokolowski, Steven Tingay, Daniel Ung, Randall Wayth
- *SKAO (International organisation)*: Mark Waterson
- *INAF (Italy)*: Pietro Bolli, Jader Monari, Federico Perini, Paola Di Ninni, Filippo Zerbi
- *IEIT, CNR (Italy)*: Giuseppe Virone
- *IDS (Italy)*: Mirko Bercigli



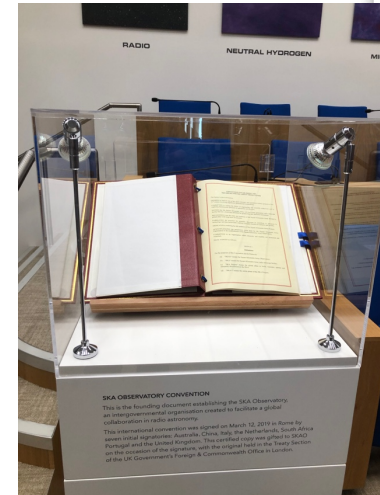
Also acknowledge former LFAA consortium members from ASTRON and Univ. of Cambridge, Oxford & Malta.

Outline

- SKA and SKA-LOW.
- SKA-LOW prototypes – history, AAVS1.5, AAVS2 and EDA2
- SKALA4 antenna
- Station level calibration
- CEM simulations (FEKO and Galileo)
- Work in progress.

The SKA project

- Square Kilometer Array is an international project to build the world's largest radio telescope.
- Project has its genesis circa 1990: *Hydrogen Array*, a proposal to image neutral hydrogen dating back to early cosmic times.
- HI is still a major driver of SKA.
- IGO treaty currently being ratified in national parliaments.

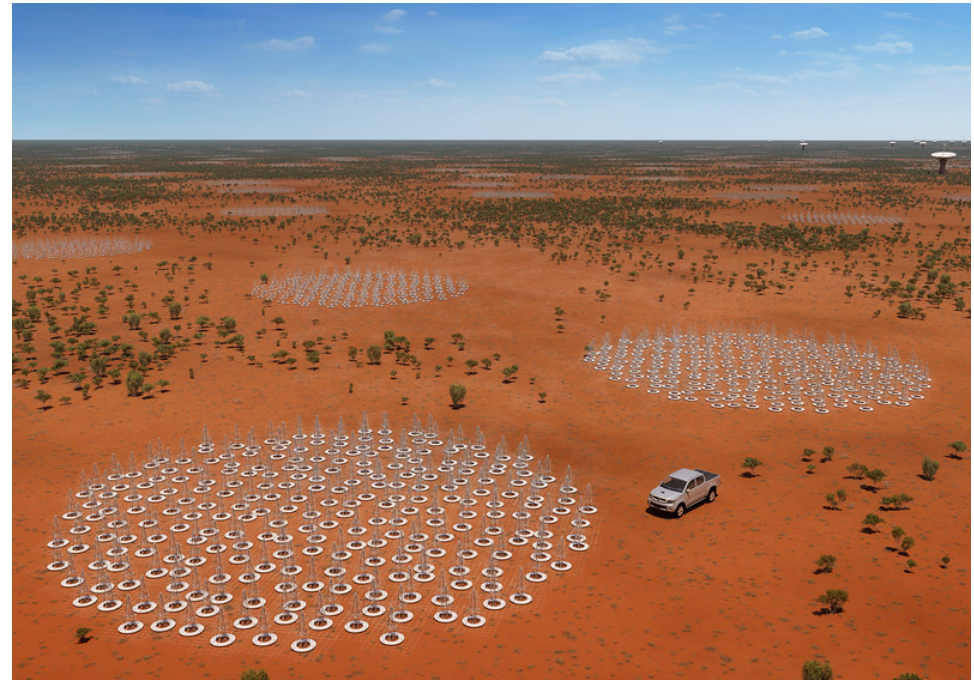


The SKA project – technical

Two main components in the field:

- SKA-MID
 - ± 200 15m dishes; Karoo (South Africa).
 - Planned to incorporate 64 dish MeerKAT.
- SKA-LOW
 - $\pm 130\ 000$ array elements (512 stations of 256 antennas, ± 40 m station diameter); Murchison Radio-astronomy Observatory (Western Australia).
 - Co-located with (but does not include) ASKAP & MWA.

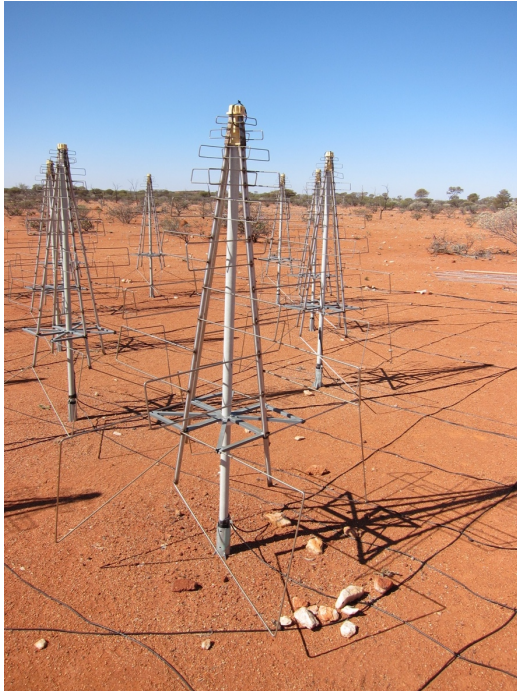
SKA-LOW



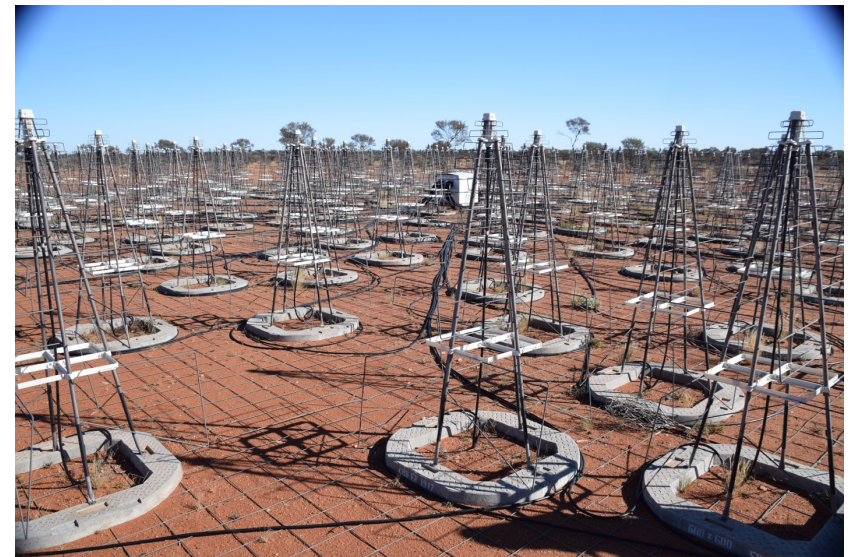
The MRO in WA – 600km NE of Perth. Murchison approx. size of NL – population ± 100 .

Artist's Image. Credit: SKAO.

SKA-LOW prototypes: Aperture Array Verification System 0.5 & 1.0



AAVS0.5: 16 SKALA elements

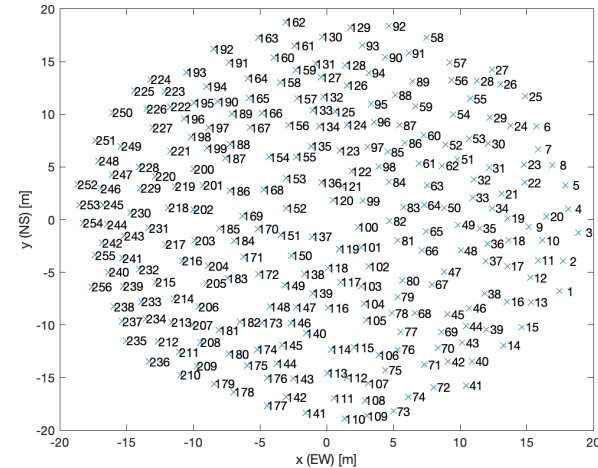


AAVS1.0: 256 element
SKALA2 elements

See also: *Exp Astron* (2018) 45:1–20, de Lera Acedo et al.

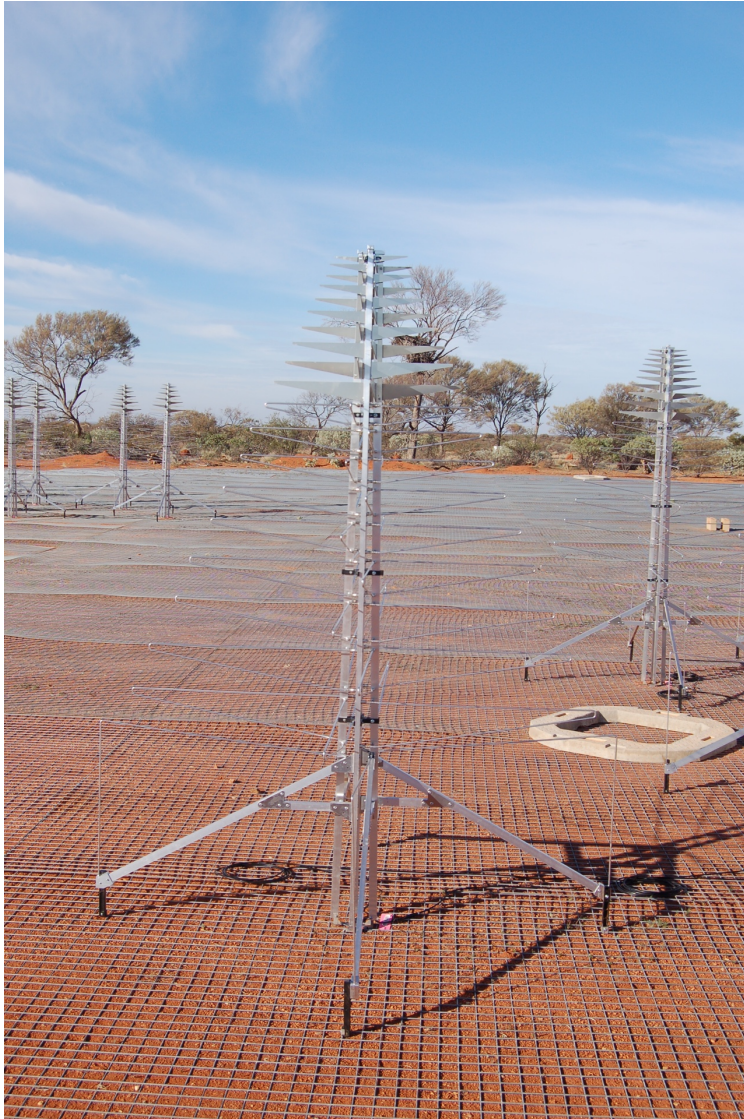
The current prototype AAVS2 (256elements) as built

- Uses SKALA4.1-AL implementation of SKALA4 reference design.
- Same quasi-random distribution as AAVS1.0, scaled radially by 7.8%, with some other minor changes (walkways etc).
- Accommodates larger footprint of the SKALA4.1.
- Deployed in phase 1 (48 antennas) and now full phase 2 (all 256).



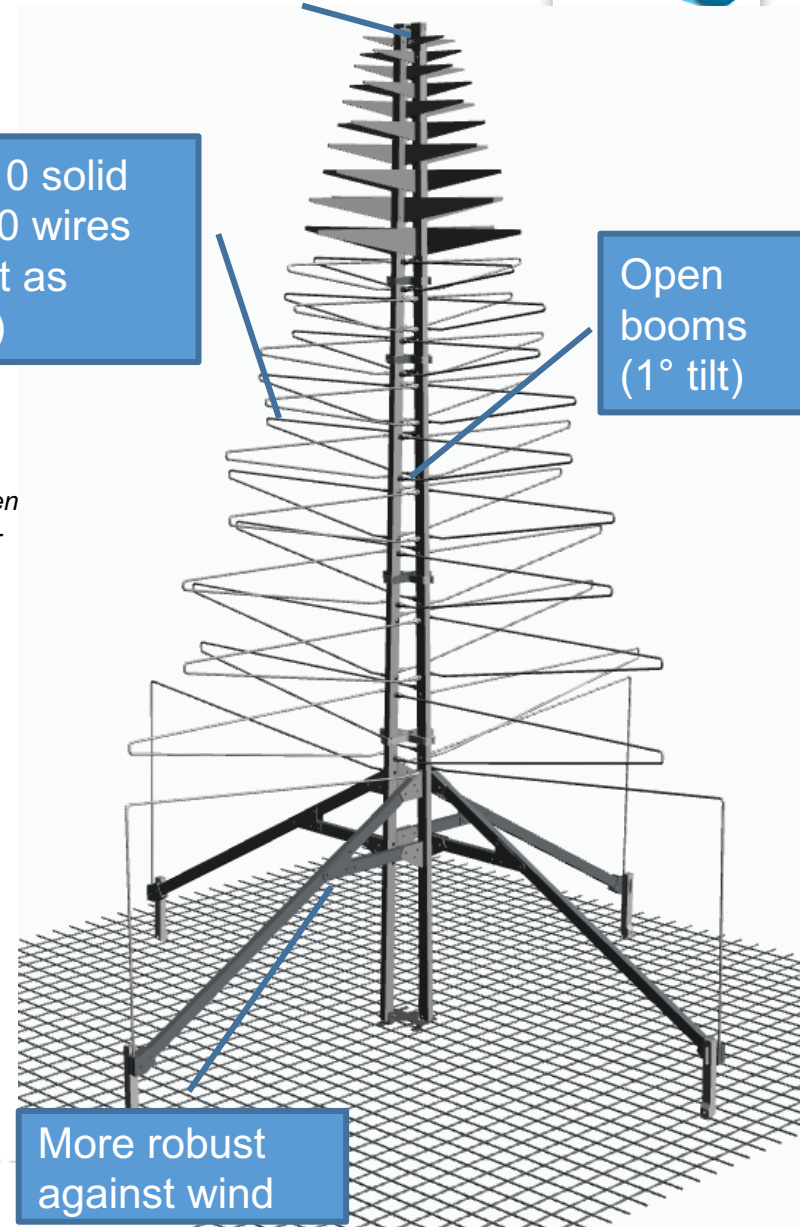
SKALA4.1-AL antenna

New LNA
connection to the
antenna feed



20 dipoles: 10 solid
dipole and 10 wires
(same height as
SKALA4-AL)

See Bolli et al, *Test-Driven
Design of an Active Dual-
Polarized Log-Periodic
Antenna for the Square
Kilometre Array*, IEEE
OJAP, June 2020



Open
booms
(1° tilt)

More robust
against wind

Simulation aims

- Compute Embedded Element Patterns (a.k.a. active, or scan element patterns) for all 256 elements (x2 for opp. pol.)
- EEPs are computed one at a time, with all other elements terminated, with a row or column of the array mutual impedance matrix Z_A computed at same time.
- EEPs are not unique – depend on termination of other elements.
- Most useful – loaded (often matched), and open-circuited.
- Transmit array beam is sum of OC EEPs.
- Receive array beam (with LNA loads taken into account) is sum of loaded EEPs.
- EEPs can be transformed mathematically between loading conditions (Warnick et al, CUP 2018 and Warnick, Davidson, provisionally accepted for IEEE Trans.AP).
- This does need Z_A .

Simulation considerations

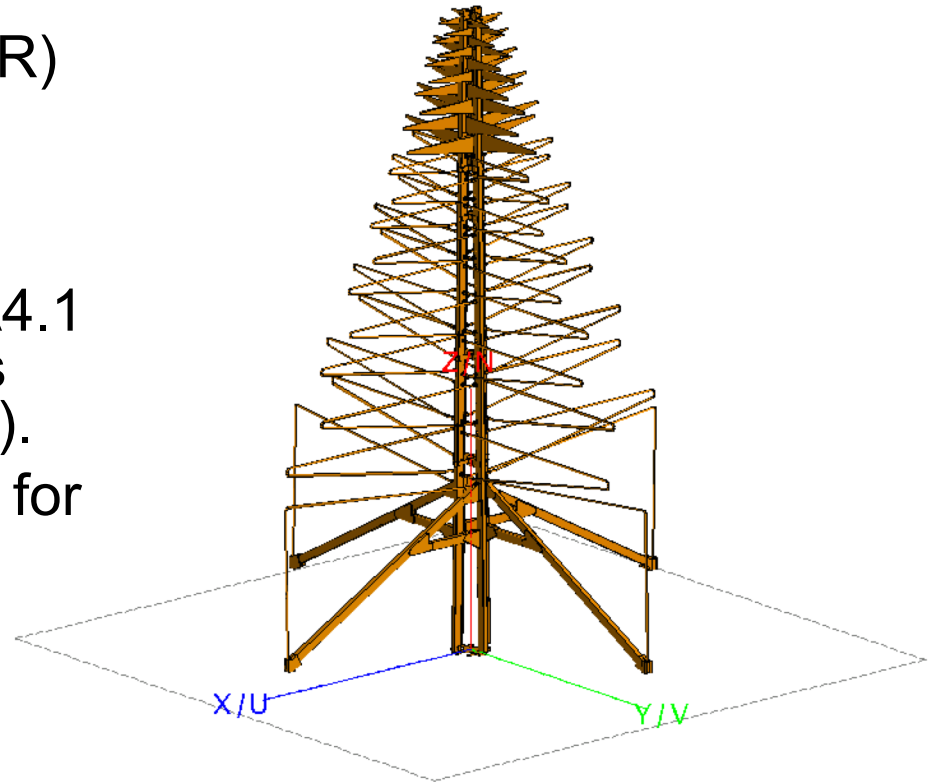
- These are large computational models.
- Cannot be solved using full Method of Moments (MoM).
- Use Multi-Level Fast Multiple Method (MLFMM) approximation.
- FEKO was first commercial code to offer this, circa 2000.
- Parallel MLFMM remains non-trivial.
- Special run-time parameter setting obtained from FEKO support to permit use of full 56 cores.
- MLFMM is an iterative method; iterations not guaranteed to converge. Issues encountered at 50 and 70 MHz.
- Typical run-times for a full 256 element station vary from days to weeks, depending on convergence of MLFMM.

Limitations of MoM/MLFMM

- No obvious way of simulating a full station with a large, finite metallic ground plane (mesh) above a semi-infinite real ground (earth) using commercial codes.
- Investigations into finite grounds have addressed single elements (later in this presentation).
- SKALA4.1 is very complex when running station simulations with 256 elements – over 3 million dofs.

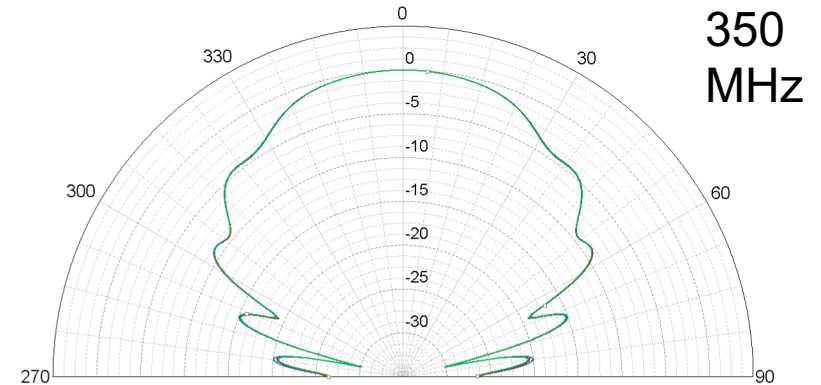
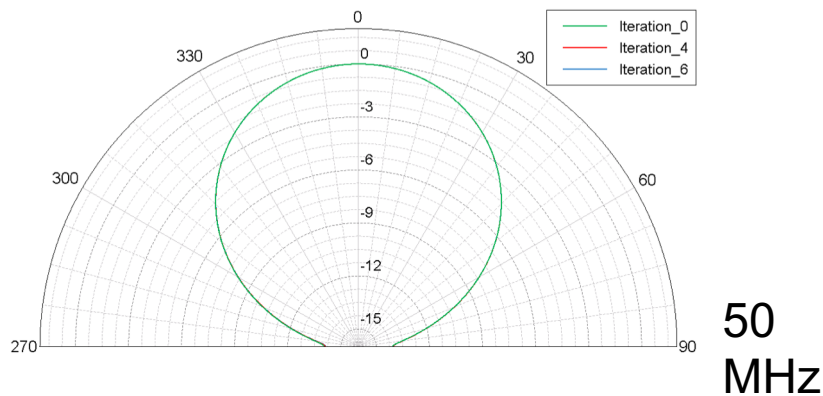
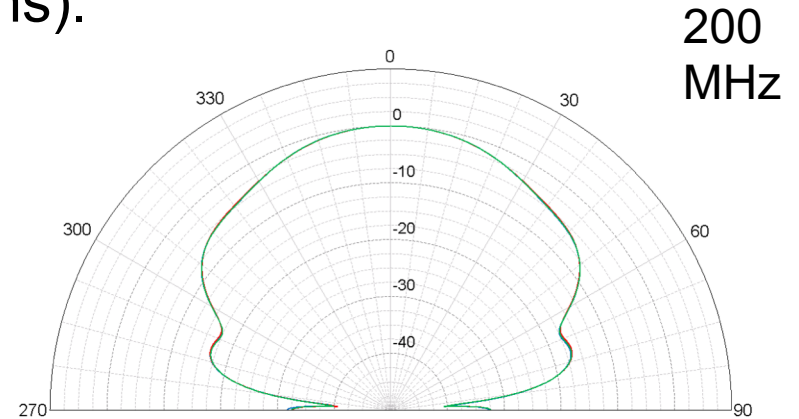
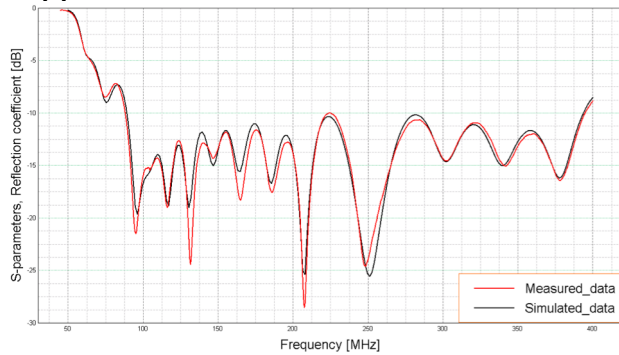
Simulation work

- Simulations used FEKO (ICRAR) and Galileo (INAF via IDS)
- SKALA4 is latest reference design.
- Usable FEKO model of SKALA4.1 obtained – approx. 12 000 dofs instead of 29 000 (per antenna).
- Large problem: $\pm 600\,000$ dofs for 48 antennas.
- IDS model uses around 9 000 dofs per antenna.
- ICRAR purchased Dell PowerEdge 740 server (56 cores, 1.5 TB RAM) for this work.
- Similar facilities at IDS.



Simulation work contd.

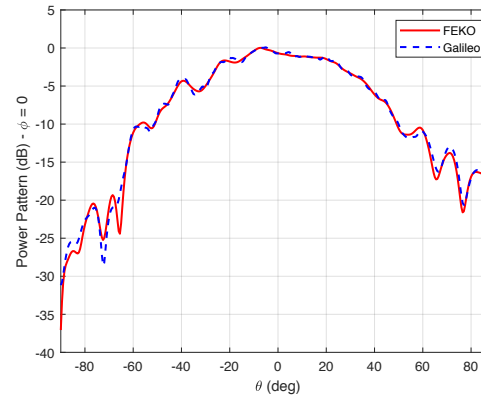
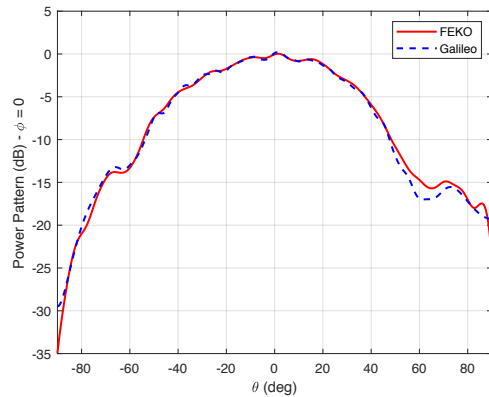
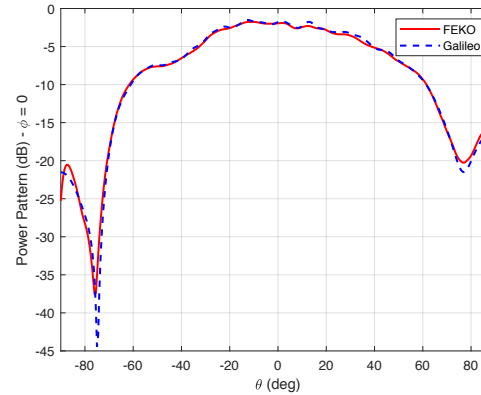
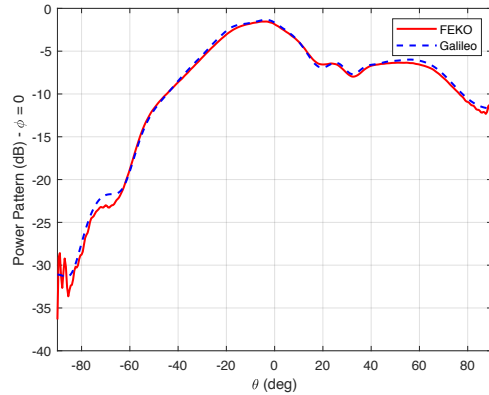
- FEKO model benchmarked against measured data (S_{11}) and full FEKO model (patterns).



Other alternatives to MLFMM

- HARP (Craye, de Lera Acedo et al):
 - Combination of primary and secondary CBFs (MBF) and a polynomial approximation of far-field coupling between MBFs.
 - Not currently available in a commercial code.
- DGF (Ludick et al):
 - Improves \propto array approx (but not presently well suited to EEP work with only one driven antenna).
 - Available in FEKO.
- Adaptive cross approximation (ACA) also in FEKO – does not work well on this problem.

Comparison of EEPs: FEKO & Galileo

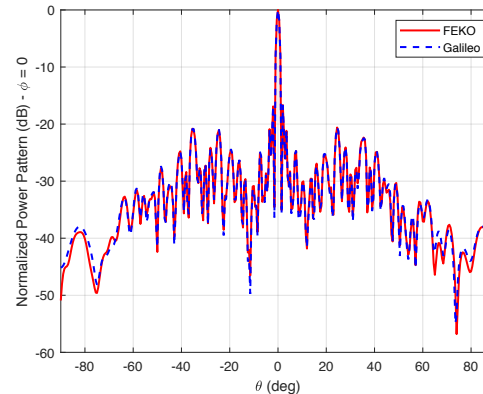
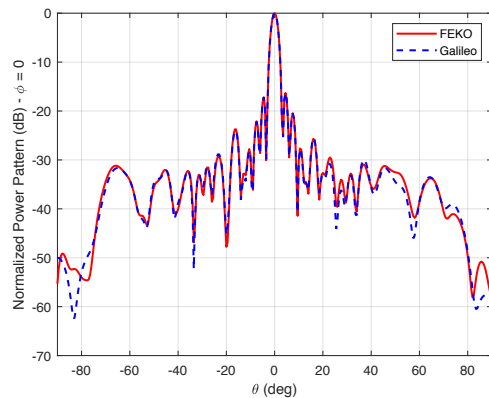
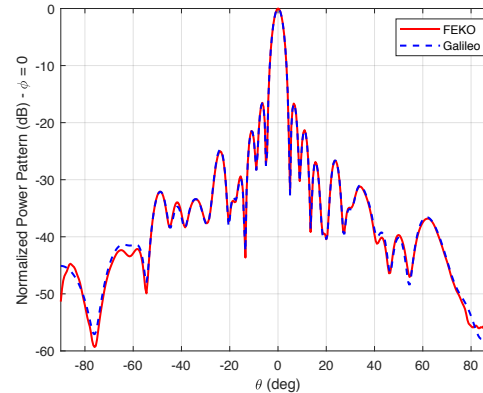
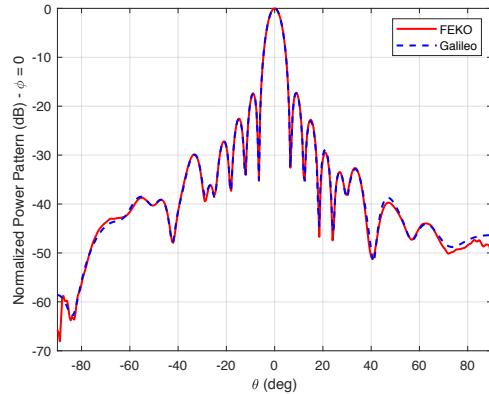


Antenna 2. EW (X) pol.

Top left: 80 MHz Top right: 110MHz

Bot left: 160 MHz Bot right: 350MHz

Zenith-pointing station beams from EEPs



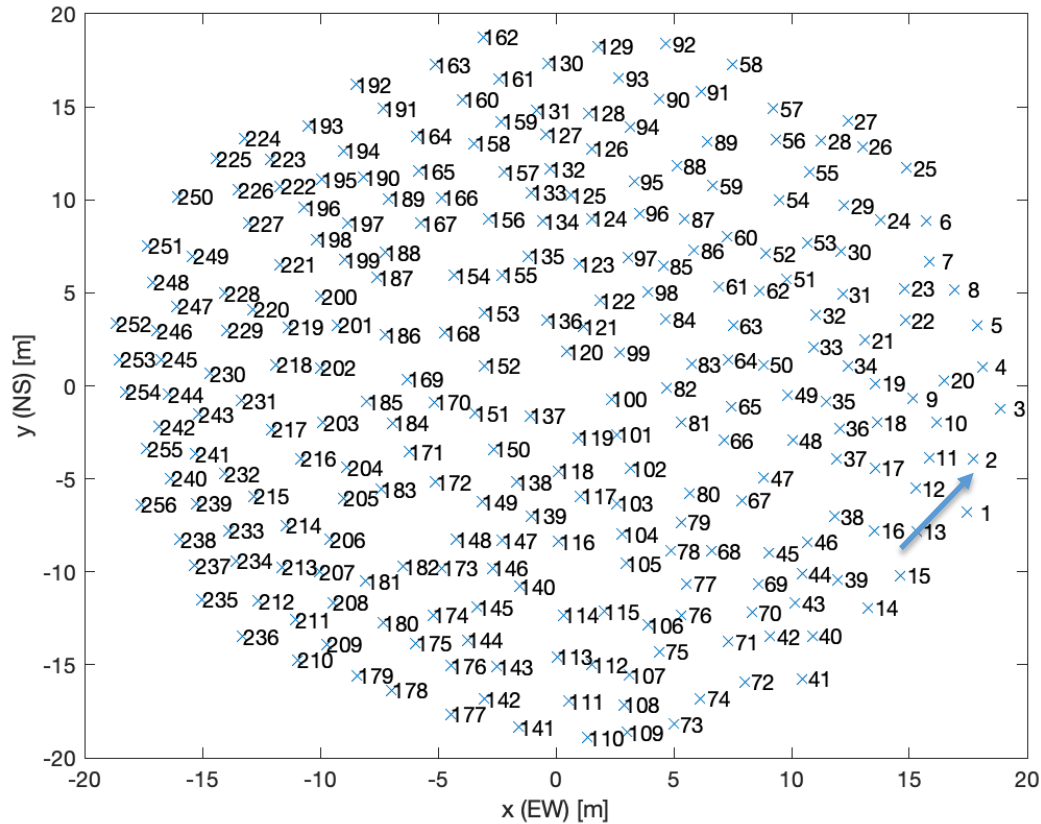
Off-zenith pointings have a slight squint issue - see later presentation.

Antenna 2. EW (X) pol.

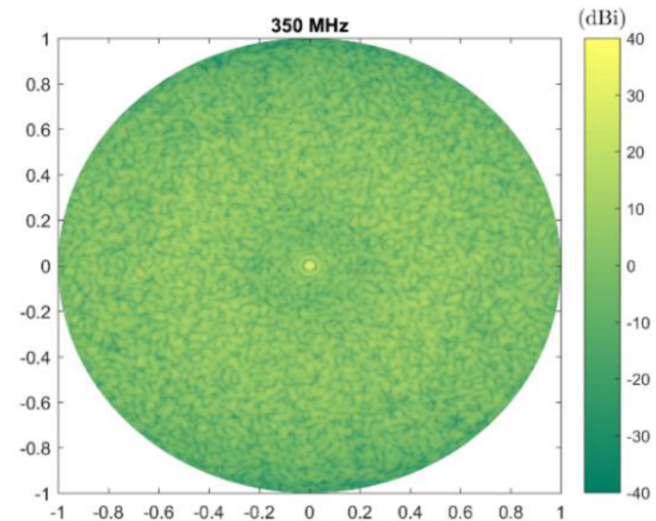
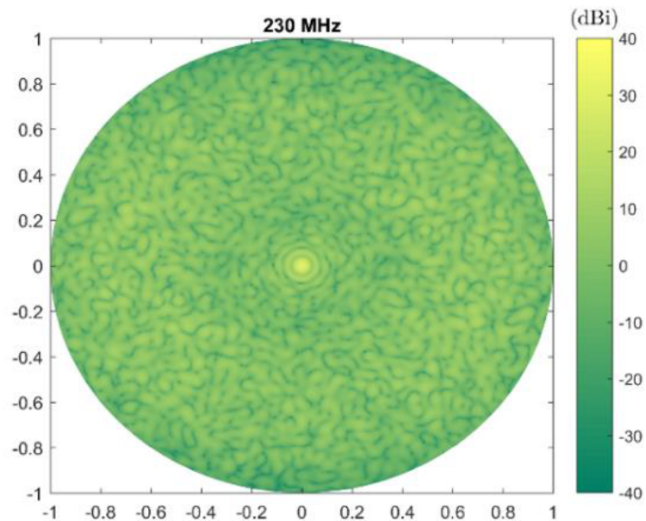
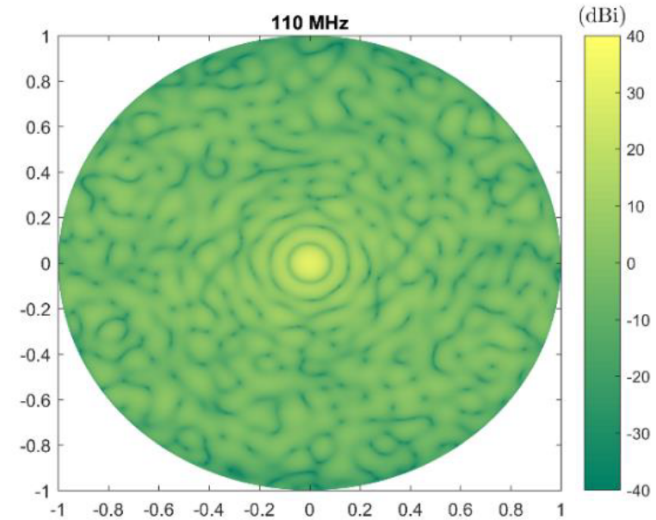
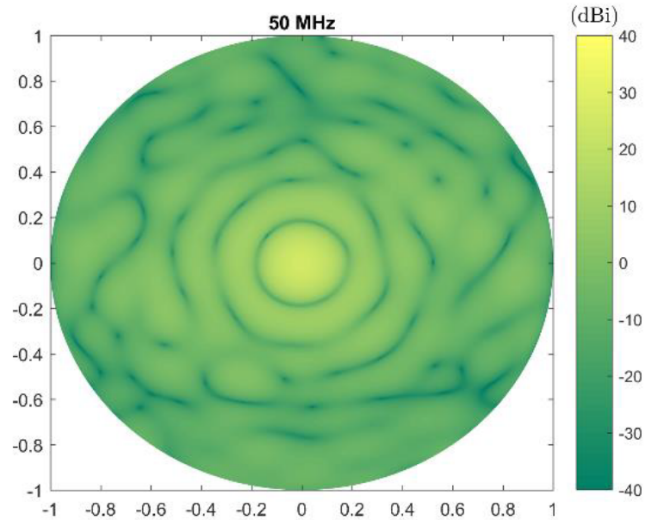
Top left: 80 MHz Top right: 110MHz

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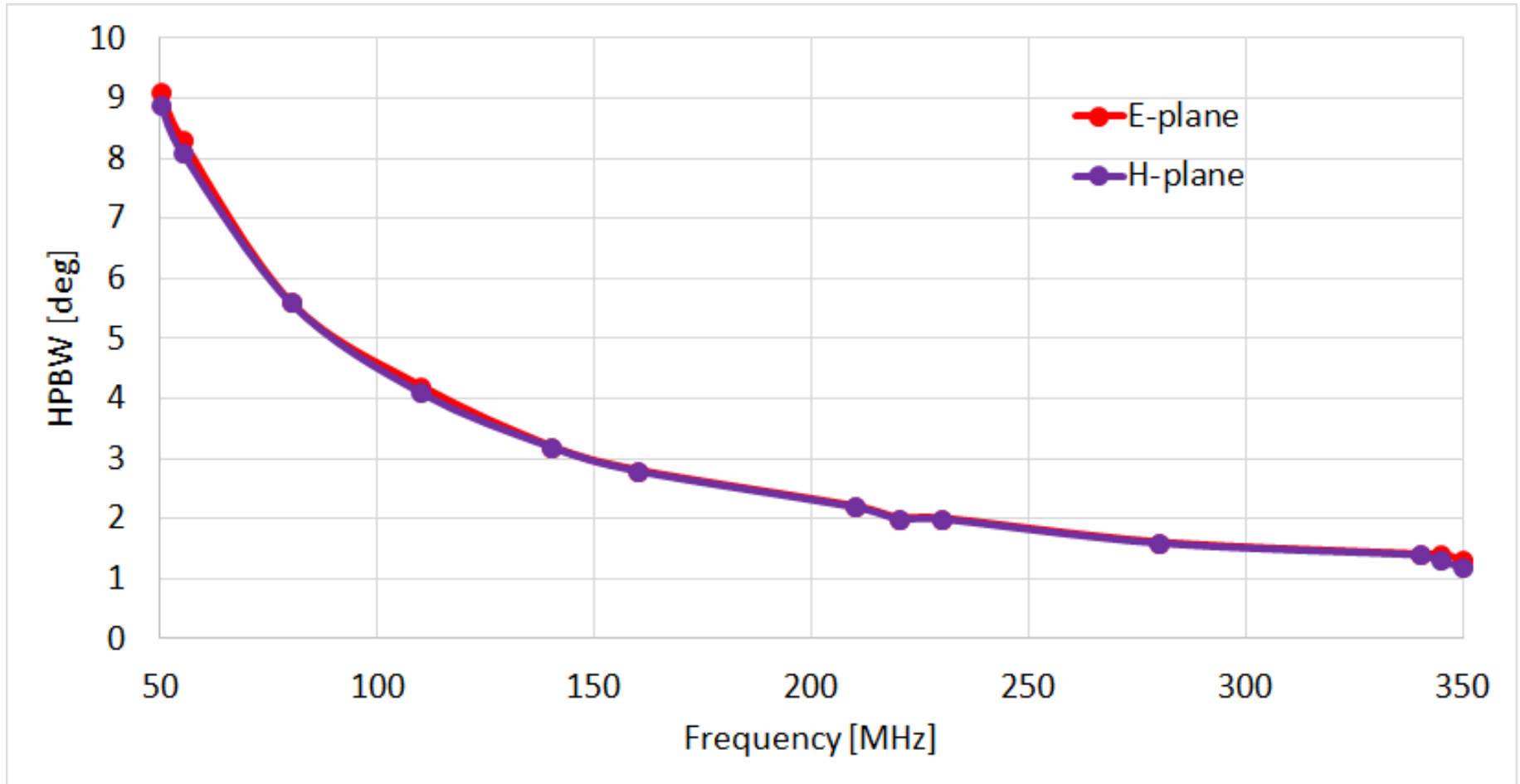
AAVS2 positions



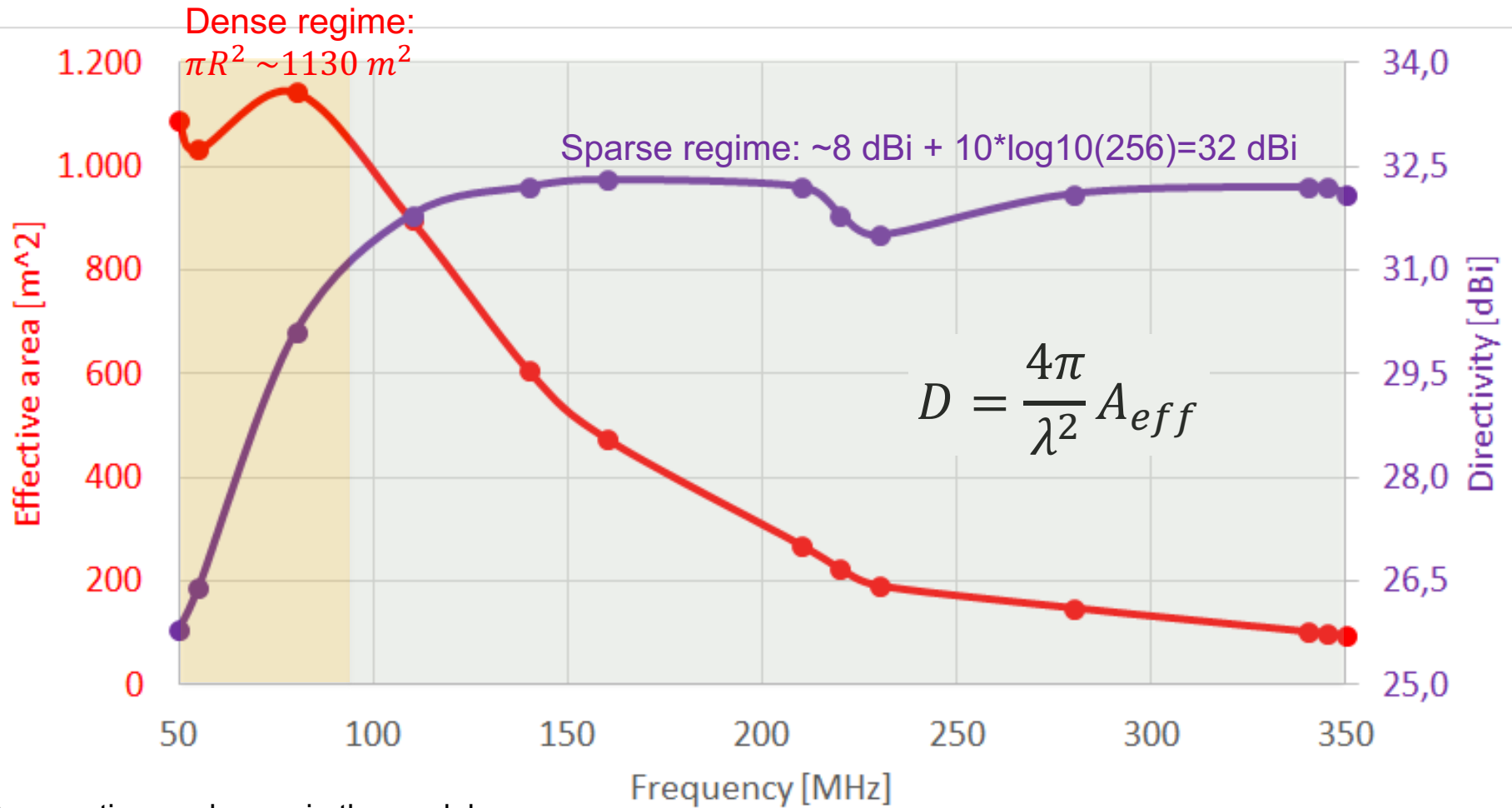
Array beam at zenith (from EEP)



Station beam HPBW at zenith

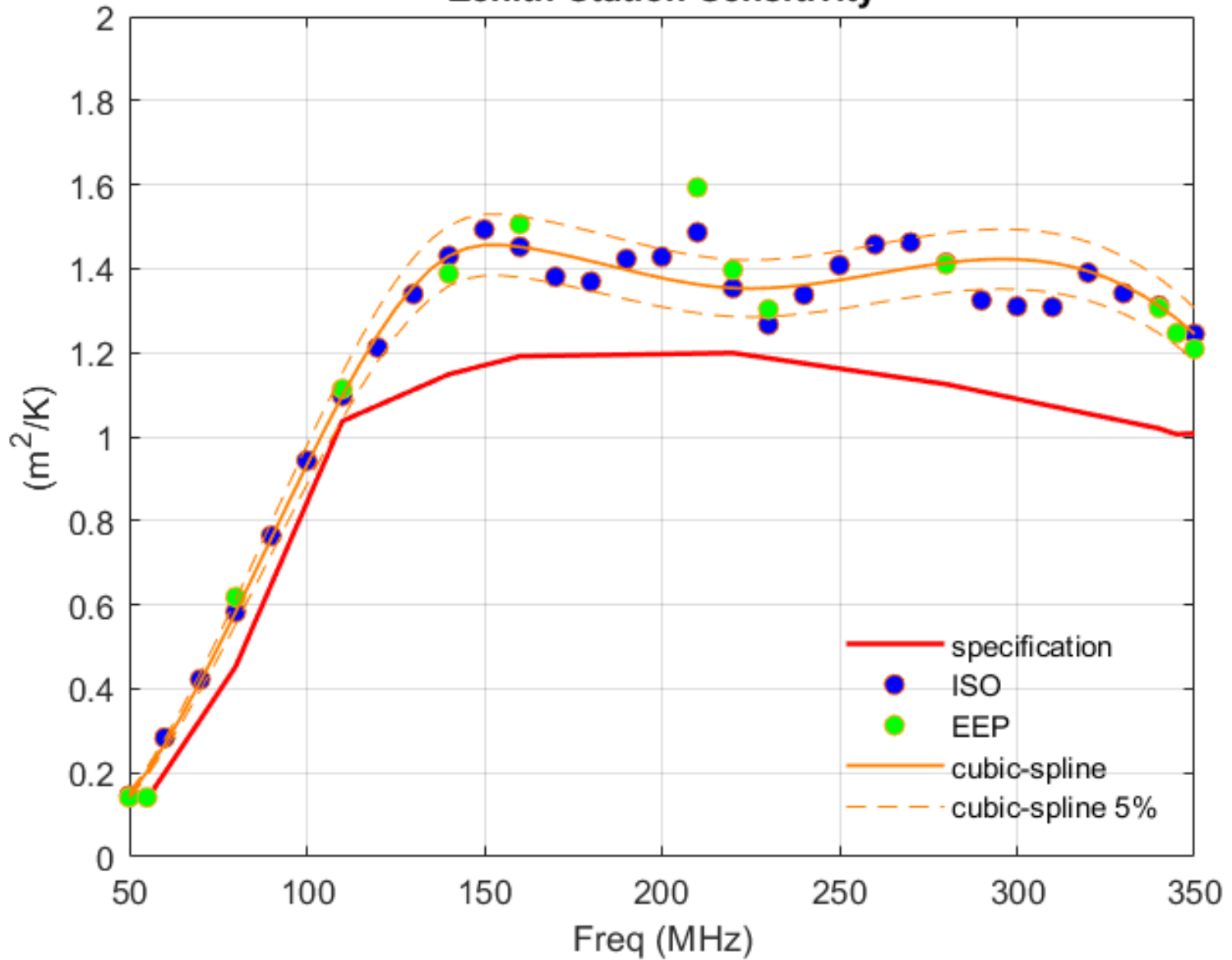


Station beam gain at zenith



Assumption: no losses in the model

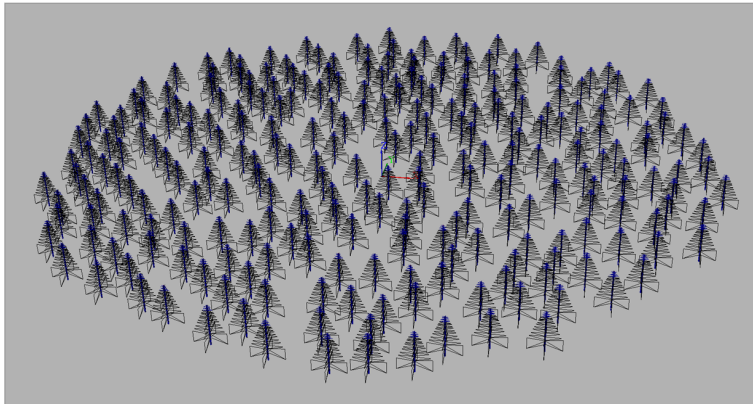
Zenith Station Sensitivity



$$Sensitivity(\vartheta, \varphi) = \eta_{Dig} \frac{A_{eff}(\vartheta, \varphi)}{T_{sys}} = \eta_{Dig} \frac{\frac{\lambda^2}{4\pi} G(\vartheta, \varphi)}{\eta_L T_{ant} + (1 - \eta_L) 290 + [T_{LNA} + \frac{T_{rx}}{G_T}]}$$

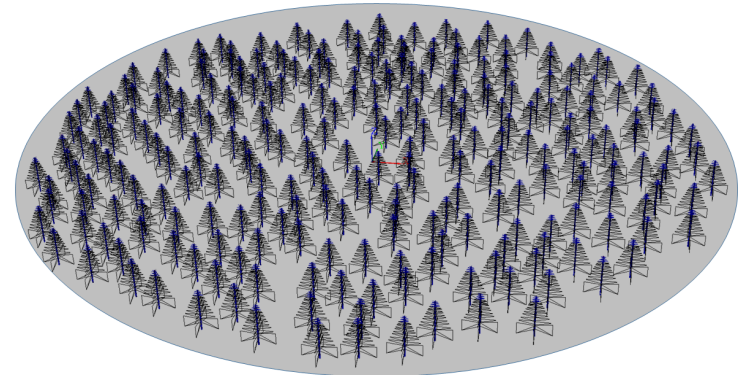
Finite real ground

Infinite ground plane



Simplified approach which allows to use the reflection coefficient approximation adding a reflected component to the field, which is a very fast technique.

Finite ground plane (42-m diameter)



More realistic scenario which allows to account for the truncation of the electrical currents induced in the ground plane and diffraction effects.

Technique for finite ground plane

Rather than using a full-wave technique, the problem of the finite ground plane is addressed through a simplified 3-step process:

- 1) computing with a full-wave approach the currents induced on the 256 antennas considering an infinite ground plane with reflection coefficient approximation;
- 2) starting from the currents of the previous point, the currents induced on a finite ground plane are computed with a full-wave approach;
- 3) the currents distributed in the antennas and in the finite ground plane are radiated applying the equivalence principle to obtain the scattered field.

More details in: P. Bolli, M. Bercigli, P. Di Ninni, M.G. Labate, G. Virone, "Preliminary Analysis of the Effects of the Ground Plane on the Element Patterns of SKA1-Low," *14th European Conference on Antennas and Propagation (EuCAP)*, (Copenhagen, Denmark), March 15-20, 2020.

Using EEPs for station calibration

- The EEPs provide the direction dependent *voltage gain* terms in the interferometric integral for dissimilar element patterns:

$$V(u, v) \approx \iint_{-\infty}^{\infty} E_p(l, m) E_q^*(l, m) e^{-j2\pi(ul+vm)} dl dm$$

- NB! It is very important to appreciate that these are **field** (i.e. voltage) gains – **complex valued**.
- This is **NOT** the usual antenna engineering usage, in which gain is a *power* based parameter.

Station calibration *contd. I*

- Direction dependent calibration is currently on the leading edge of radio astronomy practice.
- This aims to model the pattern using a simpler approximation, eg

$$E_p(l, m) \approx g_p A_p(l, m)$$
- Decompose into direction independent (DIEs) g_p (e.g. receiver gain) & direction dependent effects (DDE) $A_p(l, m)$ (element beam/EEPs; ionosphere).

- Approximate beam/EEP model:

$$A_p(l, m) = \sum_{i=1}^M \alpha_i P(l, m)$$

- Coefficients α_i are to be found; $P(l, m)$ could, for instance, be spherical harmonics, or characteristic pattern, etc.

Station calibration *contd. II*

- In principle, DIEs and DDEs can be solved during calibration, using measured visibilities & known sky map.
- However — at station level there is too little information: a-priori model of element patterns is needed.
- LOFAR and MWA adopted empirical approach; actual parameters for dipole model are not solved for.
- Wide FoV pose challenges — sky model; inclusion of w term in interferometric integral.
- 256 SKALAs \times 512 SKA-LOW stations produce 131 072 *different* EEPs — also very challenging!

Storing and using EEPs

- FEKO can store the EEPs as spherical harmonics or as a sampled radiation pattern.
- For efficiency when using SF, EEPs best phase-referenced to each individual antenna position, rather than array centre (dramatically reduces # harmonics – analogy with NF scans).
- Some post-processing is required to obtain the EEPs.
- Galileo stores sampled radiation patterns.
- If stored as a conventional radiation pattern, each set of EEPs is over one Gbyte of data at 0.5° resolution.
- Data available for SKAO use.

Conclusions

- Embedded element patterns are central to contemporary phased array analysis.
- Previous results from different groups working on SKA have been difficult to compare.
- These EEP & beam results from ICRAR & INAF teams agree well.
- Essentially a verification – both groups have used (different) MoM codes with MLFMM acceleration; both assume infinite PEC ground planes for full-station models.
- Validation addressed via an on-site drone measurement campaign – not reported here.
- Progress in CEM has made full-wave modelling *just* tractable.
- Complicated EEPs make station beam calibration difficult:
 - Mutual coupling does *not* average out for individual EEPs
 - However, the EEPs *do* average out for the array pattern.
- Modelling large aperture arrays still challenges CEM tools — scope for further work on fast methods, and including finite ground planes.

SQUARE KILOMETRE ARRAY

Exploring the Universe with the world's largest radio telescope



- End of presentation.